# ON THE HIERARCHICAL TWO-RESPONSE (CYCLIC PBIB) DESIGNS, COSTWISE OPTIMAL UNDER THE TRACE CRITERION

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### 1. Summary

Consider a general incomplete two-response design. Let  $S_1$ ,  $S_2$  and  $S_{12}$  be possible sets of units on which respectively, only response  $V_1$ , only response  $V_2$ , and both responses  $V_1$  and  $V_2$ , are to be measured. Further suppose that under each of the two sets  $(S_1 \cup S_{12})$  and  $(S_2 \cup S_{12})$ , a cyclic PBIB type of block-treatment design is going to be used. Then under a suitable cost restriction, and under the trace criterion for the comparison of designs, it is shown that the optimal two-response design will be such that at least one (and in most cases, only one) of the sets  $S_1$  and  $S_2$  would be empty. Also, methods are given to obtain the optimal design itself.

#### 2. Introduction

Consider an experimental situation with p responses  $(V_1,\cdots,V_p)$ , v treatments  $(\tau_1,\cdots,\tau_v)$  and a set  $S^*$  of experimental units, where the multiresponse design is possibly incomplete in the sense that all responses may not necessarily be measured on each experimental unit. Let  $S^*(i_1,\cdots,i_k)$  denote the subset of  $S^*$  on each element of which the responses  $V_{i_1},\cdots,V_{i_k}$  (and these alone) are measured. Thus  $U_r^*=\{S^*(i_1,\cdots,i_k)\mid r\in(i_1,\cdots,i_k)\}$  is the set of all units on which  $V_r$  is measured (alone or possibly with other responses). In a previous paper (Srivastava and McDonald [9]), heretofore, called paper I, the case where the sets  $S^*(i_1,\cdots,i_k)$  are divided into randomized blocks (of v units each) was studied. However, if v is large, or if respect to any response (say  $V_r$ ) there is a great deal of heterogeneity present in the experimental material, then as in the classical (univariate) experimental design theory, it would be advisable to use incomplete block designs rather than randomized blocks.

In paper I, it was shown that for the randomized block case, the hierarchical multiresponse (HM) (i.e. those where  $U_1^* \supseteq \cdots \supseteq U_p^*$ ) designs

are optimum in the general class of incomplete multiresponse designs, and a method of finding the optimal design was developed. In this paper, we develop a similar theory for the case when the designs defined on the set  $S^*(i_1,\dots,i_k)$  are cyclic PBIB designs of a very general type. This system of PBIB designs is very flexible in the sense that designs exist (in the combinatorial sense) for any given block size we wish. Also the number of replications of any treatment equals the block size, and therefore is not too large (unlike the BIB design in general). Of course, one could think of developing a theory of optimal multiresponse designs, where the designs on the sets  $S^*(i_1,\dots,i_k)$  are different from randomized block or cyclic PBIB designs. But this seems to necessarily involve complex combinatorial existential problems which we cannot discuss here for lack of space. Indeed, when p>2, even the cyclic PBIB gives rise to such difficulties, since the general incomplete multiresponse (GIM) design loses its structural balance. This paper is therefore restricted to p=2. Although the basic problem here is similar to that in paper I, the development is quite different. Here, the complexity arises not because of large p, but because the basic design used, viz. cyclic PBIB is mathematically more complex than the randomized blocks.

The notation is similar to that in paper I. Thus, under any design D,  $\phi(D)$  denotes the associated 'cost'. A rival design  $D^*$  is at least as good as D, if  $\phi(D^*) \leq \phi(D)$  and  $Q(D^*) \leq Q(D)$ ;  $D^*$  is 'better' if one of the inequalities is strict. Here

(2.1) 
$$Q(D) = \operatorname{trace} \left[ \operatorname{Var} \left( P \hat{\tau}^* \right) \right],$$

where  $\tau^* = (\tau'_1, \dots, \tau'_p)$ ,  $\tau'_r = (\tau_{r1}, \dots, \tau_{tv})$ ,  $\tau_{rj}$  denotes the true effect of  $\tau_j$  on  $V_r$ ,  $\tau^*$  is the best linear unbiased estimate of  $\tau^*$  under the design, and P is a  $p(v-1) \times pv$  matrix given by

(2.2) 
$$P = \operatorname{diag}(P_1, P_2, \dots, P_p)$$
,

where, for every r,  $P_r(\overline{v-1}\times v)$  is an orthonormal matrix for which the sum of the elements in every row in zero.

The designs discussed in this paper should be useful in situations where the heterogeneity in the experimental material and/or the number of treatments is large, and where the measuring costs for the two responses (or the associated variances) differ appreciably from one another.

# Determination of Q for certain response-wise incomplete cyclic PBIB designs

Consider the following cyclic PBIB design with v blocks and v treatments  $(\tau_1, \dots, \tau_v \text{ say})$ .

(3.1)	Blocks	Ι	1	2	3		(v-1)	v
		II	2	3	4	• • •	v	1
		III	3	4	5	• • •	1	2
		:	:	:	:	•••	:	:
		v	v	1	2	• • •	(v-2)	(v-1)

Suppose that two responses,  $V_1$  and  $V_2$ , are under study. Measure only  $V_1$  on the first  $k_1$  columns, both  $V_1$  and  $V_2$  on the next k columns and finally only  $V_2$  on the next  $k_2$  columns, where  $2 \le k_r + k \le v$ , (r=1, 2), and  $k_1 + k + k_2 \le v$ . Let  $D = D(k_1, k, k_2)$  denote the above "response-wise incomplete" and "treatment-wise incomplete" design. The first  $(k_1 + k)$  columns of (3.1) constitute a PBIB design  $(\text{say } D_1)$  for response  $V_1$ , and the last  $(k+k_2)$  columns form a PBIB design  $D_2$  for response  $V_2$ . Thus  $D_r$  (r=1, 2) provides  $(k+k_r)$   $(=\rho_r$ , say) replications of the set of v treatments. Assume that for both  $D_1$  and  $D_2$ , the jth associates of an element  $x \in \{1, \dots, v\}$  are  $x \pm j \pmod{v}$ . For odd v, there are ((v-1)/2+1) associate classes with, respectively,  $n_0=1$ ,  $n_1=\dots=n_{(v-1)/2}=2$  elements; and for v even, there are (v/2+1) classes with, respectively,  $n_0=1$ ,  $n_1=\dots=n_{(v/2-1)}=2$ ,  $n_{v/2}=1$  elements. Further, if any two treatments are jth associates under the design  $D_r$ , they occur together in exactly  $\lambda_{r,j}$  blocks, where

(3.2) 
$$\lambda_{r,j} = \begin{cases} \rho_r - \min(j, \rho_r); & \rho_r = 1, \dots, (v-1)/2, \\ \rho_r - \min(j, v - \rho_r); & \rho_r = (v+1)/2, \dots, v; \end{cases}$$

if v is odd; and

(3.3) 
$$\lambda_{r,j} = \begin{cases} \rho_r - \min(j, \rho_r); & \rho_r = 1, \dots, (v/2) - 1; \\ \rho_r - \min(j, v - \rho_r); & \rho_r = (v/2), \dots, v; \end{cases}$$

if v is even.

Consider now response  $V_1$  ignoring  $V_2$ . The estimate  $\hat{\tau}_1$  of  $\tau_1$  under  $D_1$  is given by the reduced normal equations  $C_1\hat{\tau}_1 = Q_1$ , where (following the notation of Kempthorne ([1], p. 80),  $Q_1$  ( $v \times 1$ ) is the vector of adjusted yields, and  $C_1$  ( $v \times v$ ) is a symmetric matrix of rank v-1 each row of which sums to zero. Also the  $(\alpha, \beta)$  element  $(\alpha, \beta=1, \dots, v)$  of  $C_1=((C_{1\alpha\beta}))$  is given by

(3.4) 
$$C_{1\alpha\alpha} = \rho_1 - 1$$
;  $C_{1\alpha\beta} = -(\rho_1^{-1})\lambda_{1\alpha\beta}$   $(\alpha \neq \beta; \alpha, \beta = 1, 2, \dots, v)$ , where  $\lambda_{1\alpha\beta} = \lambda_{1j}$  if  $|\alpha - \beta| \equiv j \pmod{v}$ . The matrix  $C_2$   $(v \times v)$  corresponding

to  $V_2$  is similarly defined with the suffix 1 replaced by 2. Now, from (2.1), we have

(3.5) 
$$Q(D) = \operatorname{tr} (\operatorname{Var} (P_1 \hat{\tau}_1)) + \operatorname{tr} (\operatorname{Var} (P_2 \hat{\tau}_2)) \\ = \sigma_{11} \operatorname{tr} (P_1 C_1^{\dagger} P_1') + \sigma_{22} \operatorname{tr} (P_2 C_2^{\dagger} P_2'),$$

where  $\sigma_{rr}$  (r=1, 2) is the variance (for response  $V_r$ ) of the observation on any experimental unit, and where  $C_r^{\dagger} = C_r^* C_r C_r^*$ ,  $C_r^*$  being a conditional inverse of  $C_r$  (i.e.  $C_r^*$  is any symmetrical matrix such that  $C_r C_r^* C_r = C_r$ ). The following lemma can be easily established.

LEMMA 3.1. If  $\theta_{rj}$  (r=1, 2) denotes the jth largest root of  $C_r$ , then

(3.6) 
$$\operatorname{tr}(P_{1}C_{1}^{\dagger}P_{1}^{\prime}) = \sum_{j=1}^{v-1} \theta_{1j}^{-1},$$

and

(3.7) 
$$Q(D) = \sigma_{11} \sum_{j=1}^{v-1} \theta_{1j}^{-1} + \sigma_{22} \sum_{j=1}^{v-1} \theta_{2j}^{-1}.$$

The next step in the evaluation of Q(D) is to find the  $\theta_{1j}$  and  $\theta_{2j}$ . Consider  $C_1$ , which is a circulant matrix in view of (3.4). Hence the roots  $\theta_{1j}$   $(j=1,\dots,v)$  of  $C_1$  are given by

$$(3.8) \quad \theta_{1j} = \begin{cases} (\rho_{1} - 1) - \rho_{1}^{-1} [\lambda_{11}(w_{j} + w_{j}^{v-1}) + \cdots \\ + \lambda_{1(v-1)/2} (w_{j}^{(v-1)/2} + w_{j}^{(v-1)/2+1})], & v \text{ odd }, \\ (\rho_{1} - 1) - \rho_{1}^{-1} [\lambda_{11}(w_{j} + w_{j}^{v-1}) + \cdots \\ + \lambda_{1,(v/2-1)} (w_{j}^{(v/2-1)} + w_{j}^{(v/2+1)}) + \lambda_{1,v/2} w_{j}^{v/2}], & v \text{ even} \end{cases}$$

where  $w_j$   $(j=1,\dots,v)$  denotes the v distinct vth roots of unity. Four cases arise. In case I, assume that v is odd and  $0 \le \rho_i \le (v-1)/2$ . Here we have

(3.9) 
$$\lambda_{l1} = \begin{cases} \rho_1 - l, & l = 1, \dots, (v - \rho_1) \\ 2\rho_1 - v, & l = (v - \rho_1 + 1), \dots, (v - 1)/2, \end{cases}$$

and

(3.10) 
$$w_j^l + w_j^{v-l} = 2\cos(2\pi j l/v) ,$$
 
$$(j=1,\dots,v-1; l=1,\dots,(v-1)/2) .$$

Thus, for  $j=1,\dots,v-1$ , we have

(3.11) 
$$\theta_{1j} = (\rho_1 - 1) - 2\rho_1^{-1} \left[ \sum_{l=1}^{v-\rho_1} (\rho_1 - l) \cos(l\alpha_j) - \sum_{l=v-\rho_1+1}^{(v-1)/2} (2\rho_1 - v) \cos(l\alpha_j) \right];$$

where  $\alpha_i = 2\pi j/v$ . The following identities are well known:

(3.12) 
$$\sum_{l=1}^{n} \cos l\alpha = \frac{\cos ((n+1)\alpha/2) \sin (n\alpha/2)}{\sin (\theta/2)},$$

(3.13) 
$$\sum_{l=1}^{n-1} l \cos l\alpha = \frac{n \sin ((2n-1)\theta/2)}{2 \sin (\theta/2)} - \frac{1 - \cos (n\theta)}{4 \sin^2 (\theta/2)}.$$

Using these identities, (3.11) simplifies to (for  $j=1,\dots,v-1$ ):

(3.14) 
$$\theta_{1j} = \rho_1^{-1} \left[ \rho_1^2 - \frac{1 - \cos(\rho_1 \alpha_j)}{1 - \cos(\alpha_j)} \right] = f(\rho_1, j), \quad \text{say}$$

For the other cases (i.e., v odd and  $\rho_1 > (v-1)/2$ , and also v even), it can be checked that the above procedure leads to equation (3.14) again, as the formula for the (v-1) nonzero roots of  $C_1$ . By the interchange of  $\rho_1$  and  $\rho_2$  we obtain the (v-1) nonzero roots  $\theta_{2j}$  of  $C_2$ . Thus, if f(x, j) is defined by (3.14) by replacing  $\rho_1$  by x  $(x=2, 3, \dots, v)$ , then (3.1) gives

(3.15) 
$$Q(D) = \sigma_{11}G(\rho_1) + \sigma_{22}G(\rho_2) ,$$

where

(3.16) 
$$G(x) = \sum_{j=1}^{v-1} [f(x, j)]^{-1}.$$

For facility in obtaining the optimum design (see Sec. 3), the function G(x),  $(x=1, 2, 3, \dots, 10, 12, 14, \dots, v)$ ,  $(v=1, 2, 3, \dots, 18, 21, 24, \dots, 45)$  is tabulated in Appendix I. For other values of v and x in this range, a good approximation can be obtained using a 4-point interpolation formula.

# 4. Optimality of the HM designs

Assume now that the 'cost' associated with the GIM design  $D_0 = D(k_1, k, k_2)$  has the structure

(4.1) 
$$\phi(D_0) = \phi_0(k_1 + k + k_2) + \phi_1(k_1 + k) + \phi_2(k_2 + k) ,$$

where  $\psi_0$  is the overhead cost of including one column of v experimental units in the experiment and  $\psi_r$ , (r=1,2), is the additional cost of measuring response  $V_r$  on the experimental units of one column. We proceed to compare  $D_0$  with the hierarchical design  $D^*=D(k_1-k_2,k+k_2,0)$  where we assume (without loss of generality) that  $k_2 \leq k_1$ . Recalling from (3.15) the value of Q(D) for any design D, we notice that  $Q(D_0)=Q(D^*)$ . Since  $\psi(D_0)-\psi(D^*)=\psi_0k_2\geq 0$ , it is clear that  $D^*$  is at least as good as  $D_0$ . This shows that the subclass of HM designs is complete within the class of GIM designs. The main problem now is to find the optimal HM design  $D^*$  for which  $\psi(D^*)=\psi'$  (a fixed positive number), and  $Q(D^*)$  is a mini-

mum. An investigation into this problem involves the following result concerning matrices, which is also of interest in the general theory of experimental designs.

THEOREM 4.1. Let  $H_1$  and  $H_2$  be  $(n \times n)$  symmetric matrices, which are respectively positive and non-negative definite. Also, for any matrix B given below, let  $\phi(B)$  be defined by

(4.2) 
$$B = \begin{bmatrix} B_1 & B_2 \\ B_3 & B_4 \end{bmatrix}, \quad \phi(B) = B_1 - B_2 B_4^{-1} B_3,$$

where B is  $(n \times n)$ ,  $B_1$  is  $(n-m) \times (n-m)$ , where n > m, and  $B_4$   $(m \times m)$  is nonsingular. Let

(4.3) 
$$\phi_1(H_1, H_2) = [\phi(H_1)]^{-1} - [\phi(H_1 + H_2)]^{-1},$$

$$\phi_2(H_1, H_2) = [\phi(H_1)]^{-1} - 2[\phi(H_1 + H_2)]^{-1} + [\phi(H_1 + 2H_2)]^{-1}.$$

Then  $\phi_1(H_1, H_2)$  and  $\phi_2(H_1, H_2)$  are positive semidefinite.

PROOF. Define  $\phi_1^* = H_1^{-1} - (H_1 + H_2)^{-1}$  and  $\phi_2^* = H_1^{-1} - 2(H_1 + H_2)^{-1} + (H_1 + 2H_2)^{-1}$ . Since,  $\phi_i(H_1, H_2)$  is a principal submatrix of  $\phi_i^*$  (i=1, 2), the result will be proved if the  $\phi_i^*$  are both p.s.d. Now, there exists a nonsingular matrix T such that  $H_i = TE_iT'$ , where  $E_i$  are diagonal matrices with non-negative elements, and  $E_1$  is nonsingular. Hence, putting  $\Delta_1 = E_1^{-1} - (E_1 + E_2)^{-1}$ , and  $\Delta_2 = E_1^{-1} - 2(E_1 + E_2)^{-1} + (E_1 + 2E_2)^{-1}$ , we have  $\phi_i^* = T'^{-1}\Delta_iT^{-1}$ . Thus it is enough to show that the  $\Delta_i$  are p.s.d. However, if  $e_{ji}$  and  $\delta_{ji}$  respectively represent the jth diagonal element of  $E_i$  and  $\Delta_i$  for (i=1, 2), then  $\delta_{j1} = e_{j1}^{-1} - (e_{j1} + e_{j2})^{-1}$ ,  $\delta_{j2} = e_{j1}^{-1} - 2(e_{j1} + e_{j2})^{-1} + (e_{j1} + 2e_{j2})^{-1}$ . Thus  $\delta_{j1} \ge 0$ ,  $\delta_{j2} \ge 0$ , and the proof is completed.

Consider now one response, and three disjoint sets  $U_i$  (i=1, 2, 3) of experimental units. Here all units of all sets are assumed mutually independent, and any observation on any unit has the same variance  $\sigma^2$ . Let  $U_i$  give rise to a vector of (independent) observations  $y_i$ , and let

(4.4) 
$$E(y_1) = A_1 \tau^* + A_2 \beta^*, \quad E(y_2) = E(y_3) = A_3 \tau^* + A_4 \beta^*,$$

where  $\tau^*$  and  $\beta^*$  are unknown parameters, which without any essential loss of generality can be assumed to be estimable from  $y_i$ . Let  $U_i^* = U_1$ ,  $U_i^* = U_1 + U_2$ ,  $U_3^* = U_1 + U_2 + U_3$ ; where + denotes union. Let  $\hat{\tau}_i^*$  denote the best linear unbiased estimate of  $\tau^*$  obtained from the observations on the units in  $U_i^*$  (i=1,2,3). Then  $W_i$ , the variance-matrix of  $\hat{\tau}_i^*$  is given by  $W_i = [\phi(H_i^*)]^{-1}$ , where  $H_1^* = H_1$ ,  $H_2^* = H_1 + H_2$ , and  $H_3^* = H_1 + 2H_2$ , and where

(4.5) 
$$H_{1} = \begin{bmatrix} A'_{1}A_{1} & A'_{1}A_{2} \\ A'_{2}A_{1} & A'_{2}A_{2} \end{bmatrix}, \qquad H_{2} = \begin{bmatrix} A'_{3}A_{3} & A'_{3}A_{4} \\ A'_{4}A_{3} & A'_{4}A_{4} \end{bmatrix}.$$

In this context, Theorem 4.1 tells us that the matrices  $\phi_i$ , where  $\phi_1 = (W_1 - W_2)$  and  $\phi_2 = [(W_1 - W_2) - (W_2 - W_3)]$  are both positive definite. Now  $W_1 - W_2$ , and  $(W_2 - W_3)$  can be interpreted as the "decrease in the variance" due to the addition of  $U_2$  or  $U_3$ . (Note that  $U_2$  and  $U_3$  are, in view of (4.4), 'equivalent' sets of units.) Thus  $\phi_1$  being p.s.d. means "variance decreases" by the addition of  $U_2$ , and  $\phi_2$  p.s.d. implies that 'variance' has the 'convexity property' in the generalized sense that the 'decrease in variance' is 'more' at the first addition of  $U_2$ , than at the next addition of the equivalent set of units  $U_3$ .

Notice that  $\phi_1$  being p.s.d. implies  $\operatorname{tr} W_1 \ge \operatorname{tr} W_2$ . Recalling the definition of G(x) from (3.16), this gives

(4.6) 
$$G(x) \ge G(x+1)$$
,  $x=2, 3, \dots, v-1$ .

Again, suppose in the above discussion, we let the first x columns of (3.1) correspond to  $U_1$ , the (x+1)th column to  $U_2$ , and the (x+2)th column to a new set  $U_3'$ . Notice that  $U_2^*$  would then involve the first (x+1) columns, and  $U_3^*$  will be  $U_2^*$  with the (x+1)th column occuring twice. Let  $U_3^{**}$  correspond to the first (x+2) columns. Assume there is only one response. Let  $\Gamma_1$  and  $\Gamma_2$  respectively be the covariance matrix  $\operatorname{Var}(P_1\hat{\tau}_1)$  based on the designs  $U_3^*$  and  $U_3^{**}$ . Then (recall (3.14))  $[f(x+2,j)]^{-1}$  is the jth root of  $\Gamma_2$ . Also, correspondingly the jth root of  $\Gamma_1$  is  $[f^*(x+2),j)]^{-1}$  where

$$f^*(x+2, j) = (x+2) - (x+2)^{-1} \lambda_{2j}$$

(4.8) 
$$\lambda_{2j} = 2 + \frac{\sin[(x+1/2)\alpha_j]}{\sin(\alpha_j/2)} + \frac{1 - \cos[(x+1)\alpha_j]}{2\sin^2(\alpha_j/2)}$$

with  $\alpha_j = 2\pi j/v$ . A proof of this is out of place here, and would be found in McDonald [3]. Thus it is easily checked that  $[f(x+2, j)]^{-1} \leq [f^*(x+2, j)]^{-1}$ , for all permissible j. This shows that our method of using a new column is better than repeating the same column more than once.

Furthermore, we now show that  $U_3^{**}$  (like  $U_3^{*}$ ) also has a kind of convexity property.

THEOREM 4.2. Let  $h(x, j) = (1 - \cos \alpha_j) f(x, j)$ , where  $\alpha_j = 2\pi j/v$ ;  $j = 1, 2, \dots, v-1$ ; and  $x=2, 3, \dots, v$ . Then for all permissible x and j, we have

$$(4.9) [h(x,j)]^{-1} - [h(x+1,j)]^{-1} \ge [h(x+1,j)]^{-1} - [h(x+2,j)]^{-1}.$$

PROOF. Let  $\zeta_1(x) = h(x+2, j)[h(x+1, j)-h(x, j)]$ ,  $\zeta_2(x) = h(x, j)[h(x+2, j)-h(x+1, j)]$ , and  $\zeta_3(x) = \zeta_1(x)-\zeta_2(x)$ . Then it is enough to show that  $\zeta_3(x) \ge 0$ . Let  $\cos \alpha_j = c$ ,  $\sin \alpha_j = s$ ,  $\cos \alpha_j(x+1) = c_1$ , and  $\sin \alpha_j(x+1) = s_1$ ; and  $\zeta_4(x) = (1/2)x(x+1)\zeta_3(x)$ . Then it can be checked that

(4.10) 
$$\zeta_4(x) = (1-c)(1-c_1)x^2(x+2)(x+1)^{-1} + (1+c_1)(1-c)^2x(x+2) + (1-c_1^2) + (1-c^2) + (1-cc_1)(2-c_1-3c) - 3ss_1(1-c)(x+1) - ss_1(1-c_1)(x+1)^{-1}.$$

Note that  $\zeta_4(0)=0$ . Thus it is enough to show that  $\zeta_5(x)\geq 0$ , where  $\zeta_5(x)=\zeta_4(x+1)-\zeta_4(x)$ , for  $x=0,\dots,v-3$ . Putting  $\varepsilon_x=(x+1)^{-1}(x+2)^{-1}$  we find

(4.11) 
$$\zeta_{5}(x) = (1-c)(1-c_{1})[(2x+2)-\varepsilon_{x}]+(1+c_{1})(1-c)^{2}(2x+3) + ss_{1}(1-c_{1})\varepsilon_{x}-3ss_{1}(1-c).$$

We consider three cases. In case 1, assume  $ss_1=0$ ; then clearly  $\zeta_5(x) \ge 0$ . In case 2, assume  $ss_1<0$ . The only negative term in  $\zeta_5(x)$  is  $ss_1(1-c_1)\varepsilon_x$ . Let

(4.12) 
$$\zeta_{\theta}(x) = (1-c)^{-1}(1-c_1)^{-1}\zeta_{5}(x)$$

$$= (2x+2-\varepsilon_{x}) + (2x+3)(1+c_1)(1-c)/(1-c_1)$$

$$-3[ss_{1}/(1-c_{1})] + \varepsilon_{x}ss_{1}/(1-c) .$$

Now  $|\varepsilon_x ss_1/(1-c)| \le |\varepsilon_x \sin 2(x+1)\gamma_j(\sin \gamma_j)^{-1}|$ , where  $\gamma_j = \pi j/v$ . Since  $|\sin u\theta| (\sin \theta)^{-1} |\le u$  when u is positive, we have  $|\varepsilon_x ss_1(1-c)^{-1}| \le \varepsilon_x 2(x+1)$ . Thus  $\zeta_6(x) \ge (2x+2) - \varepsilon_x - \varepsilon_x (2x+2) > 0$ . In the third and final case, assume  $ss_1 > 0$ . Consider

(4.13) 
$$\zeta_{7}(x) = (2x+3)(1+c_{1})(1-c)(1-c_{1})^{-1} - 3ss_{1}(1-c_{1})^{-1}$$
$$= (2x+3)(1-c)u^{2} - 3su,$$

where  $u=\cot(x+1)\pi j/v$ . Consider  $\zeta_7(x)$  as a function of u and call it  $\zeta_7^*(u)$ . Differentiating  $\zeta_7^*(u)$  with respect to u, we find that  $\zeta_7^{*'}(u)=2(2x+3)(1-c)u-3s=0$  implies that  $u=u_0$  (say)=3s/2(2x+3)(1-c). Secondly,  $\zeta_7^{*''}(u_0)=2(2x+3)(1-c)\geq 0$ , so the minimum value of  $\zeta_7^*(u)$ , under variation of u, is  $\zeta_7^*(u_0)=-9s^2/4(2x+3)(1-c)=[-9\cos^2\gamma_j]/[2(2x+3)]$ . Now  $\zeta_5(x)\geq (2x+2)-\varepsilon_x-9\cos^2\gamma_j/2(2x+3)\geq (2x+2)-\varepsilon_x-9/2(x+3)$ . Thus  $\zeta_5(x)\geq 0$  for  $x=0,1,2,\cdots,v$ . This completes the proof.

We now return to the problem of the determination of the optimum HM design assuming that the variances  $\sigma_{11}$  and  $\sigma_{22}$  are known (or good estimates are available) and that  $\psi_0$ ,  $\psi_1$ ,  $\psi_2$  are given. The problem is to find the design  $D^*=D(k_1,k,k_2)$  which minimizes Q, defined in equation (3.15), subject to the linear constraints  $2 \leq k_r + k$ , (r=1,2),  $k_1 + k_2 + k \leq v$  and  $\psi(D^*) \leq \psi'$ , where  $\psi'$  is the total capital available for conducting the experiment. Since the subclass of HM designs is complete the procedure will be to evaluate Q for the optimum HM design of the type  $D(k_1, k, 0)$  and compare it with Q evaluated for the optimum design of the type  $D(0, k, k_2)$ . In what follows, we let

$$(4.14) \gamma_1 = \phi_0 + \phi_1, \gamma_2 = \phi_0 + \phi_2, \gamma_{12} = \phi_0 + \phi_1 + \phi_2,$$

and denote by [x], the largest integer less than or equal to x. Also, to avoid unessential complications, we make the (mild) assumption that  $N=\phi'/\gamma_{12}$  is an integer.

Two cases arise. Under case I, assume  $k_2=0$ . Now  $k \le N$ . Let N-k=m, then  $k_1=m+\lceil m\psi_2/\gamma_1 \rceil$ . For any given m, denote the corresponding HM design D by  $D_{1,m}$ . The problem is to find the optimum value of m. Since the optimum HM design must be connected with respect to response  $V_2$ , we must have  $\rho_2=k\ge 2$ . Thus the admissible values of m are  $m=0,1,\cdots,N-2$ .

Now

(4.15) 
$$Q(D_{1,m}) = \sigma_{11}G(N + [m\psi_2/\gamma_1]) + \sigma_{22}G(N-m).$$

Thus  $Q(D_{1,m}) \leq Q(D_{1,m+1})$ , if and only if

$$(4.16) \quad \frac{\sigma_{22}}{\sigma_{11}} \ge \frac{G(N + [m\phi_2/\gamma_1]) - G(N + [(m+1)\phi_2/\gamma_1])}{G(N - (m+1)) - G(N - m)} = \beta_{1,m} , \quad \text{(say)}.$$

Now consider subcase Ia where  $\psi_2/\gamma_1 \ge 1$ . Here  $[(m+1)\psi_2/\gamma_1] - [m\psi_2/\gamma_1] \ge 1$ . Hence by (4.6) and (4.9),  $\beta_{1,m}$  is a monotone decreasing function of m and

(4.17) 
$$\max_{m} \beta_{1,m} = \beta_{1,0} = \frac{G(N) - G(N + [\psi_2/\gamma_1])}{G(N-1) - G(N)}.$$

Hence if  $\sigma_{22}/\sigma_{11} \ge \beta_{1,0}$ , then  $D_{1,0} = D(0, N, 0)$  is optimum. If  $\sigma_{22}/\sigma_{11} < \beta_{1,0}$  then  $D_{1,m_0} = D(m_0 + [m_0 \psi_2/\gamma_1], N - m_0, 0)$  is optimum where  $m_0$  is the least value of m for which  $\sigma_{22}/\sigma_{11} \ge \beta_{1,m}$ . If  $\sigma_{22}/\sigma_{11} < \beta_{1,N-3}$  then  $D_{1,N-2}$  is optimum. For subcase Ib, where  $\phi_2/\gamma_1 < 1$  the procedure is more complicated since  $\beta_{1,m}$ is no longer a monotone function of m. However,  $[(m+1)\psi_2/\gamma_1]-[m\psi_2/\gamma_1]$  $\gamma_1 \leq 1$ . Thus when  $[(m+1)\phi_1/\gamma_1] = [m\phi_1/\gamma_1]$ , we have  $\sigma_{22}/\sigma_{11} > \beta_{1,m} = 0$ , and  $D_{1,m}$  is better than  $D_{1,m+1}$ . The procedure is to find the set M of values of  $m=0, 1, \dots, N-2$  such that  $[(m+1)\psi_2/\gamma_1]-[m\psi_2/\gamma_1]=1$ . Let  $M=\{m_{i_1}, \dots, m-1\}$  $\cdots$ ,  $m_{i_l}$  where  $m_{i_1} < m_{i_2} < \cdots < m_{i_l}$ . By (4.6) and (4.9)  $\beta_{i, m_{i_1}} \ge \beta_{i, m_{i_2}} \ge \cdots \ge 1$  $\beta_{1,m_{i_1}}$ . If  $\sigma_{22}/\sigma_{11} \ge \beta_{1,m_{i_1}}$  or M is empty, then  $D_{1,0}$  is optimum. If  $\sigma_{22}/\sigma_{11} < 1$  $\beta_{1,m_i}$  then find the smallest value of  $m \in M$ , (say)  $m_{i_h}$ , such that  $\sigma_{22}/\sigma_{11} \ge$  $\beta_{1,m_{i_h}}$ . If  $\sigma_{22}/\sigma_{11} < \beta_{1,m_{i_l}}$  then set h-1=l in the following. Evaluate Q for the designs  $D_{1,m}$  corresponding to the values of m equal to  $(m_{i_{n-1}}+1)$ ,  $(m_{i_{n-2}}+1), \cdots, (m_{i_1}+1)$  and 0 and select the one for which Q is a minimum. Clearly, in practice this number (h-1) should be expected to be Hence using Appendix I, the evaluation of Q and their comparison would be quite easy.

For case II, assume  $k_1=0$ . Subcases II a  $(\phi_1/\gamma_2 \ge 1)$  and II b  $(\phi_1/\gamma_2 < 1)$  arise as for case I. Exactly the same results as above, with the sub-

scripts 1 and 2 interchanged, are applicable.

The procedure that suggests itself is to obtain the best design from each of cases I and II and compare Q calculated for each. Usually this procedure can be shortened.

If  $\phi_2/\gamma_1 < 2$  and  $\phi_1/\gamma_2 < 2$  (as will be the case in most applications), then by (4.6) and (4.9), all of the  $\beta$ 's in cases I and II are less than 1. Thus if  $\sigma_{22}/\sigma_{11}=1$ , the optimum design is  $D^*=D(0, N, 0)$ . If  $\sigma_{22}/\sigma_{11}<1$ , then the optimum design will come from case I, while if  $\sigma_{11}/\sigma_{22}<1$  the optimum design will come from case II.

If  $\psi_1/\gamma_1 \ge 2$ , but  $\beta_{10} \le 1$ , the same remarks as in the preceding paragraph are applicable. However if  $\beta_{10} > 1$ , we must compare the optimum designs from each of cases I and II. A similar remark as above with the subscripts 1 and 2 interchanged is also applicable.

Example. We now illustrate the preceding theory using some artificial data. Suppose that v=40 varieties of wheat are to be compared with respect to two responses:  $V_1$ =total yield of grain in lbs. per acre and  $V_2$ =total yield, in terms of protein, in lbs. per acre. Assume that it is known from past experience that  $\sigma_{11}=32,400$ ,  $\sigma_{22}=3,600$ ,  $\phi_1=40$ ,  $\phi_2=600$ , and  $\phi_0=800$ . Further assume that  $\phi'=7,200$ , so that if the SM design is used we will have  $N=\phi'/\gamma_{12}=5$  replications of each variety. Now  $\phi_2/\gamma_1=600/840<2$ ,  $\phi_1/\gamma_2=40/1400<2$ , and  $\sigma_{22}/\sigma_{11}=.11<1$  so that the optimum design will come from case I (i.e.,  $k_2=0$ ). Also since  $\phi_2/\gamma_1<1$  we are under subcase Ib. The admissible values of m such that  $m_1=1$  and  $m_2=1$ . From (4.16) and using Appendix I, we get  $\beta_{1,1}=.157$  and  $\beta_{1,2}=.017$ . Thus  $(\beta_{1,1}=.157)>(\sigma_{22}/\sigma_{11}=.11)>(\beta_{1,2}=.017)$ , and we evaluate Q corresponding to  $m=m_{i_1}+1=2$  and m=0. Using (4.15) and Appendix I, we have  $Q(D_{1,0})=674,100$  and  $Q(D_{1,2})=664,815$ . Thus the optimum design is  $D_{1,2}=D(3,3,0)$ .

# Appendix I

Values of the Function G(x),  $(x=1, 2, \dots, 10, 12, 14, \dots, V)$ .

```
G(2) = 1.333 G(3) = .667
V = 3
         G(2) = 2.500 G(3) = 1.125 G(4) = .750
V = 4
         G(2) = 4.000 G(3) = 1.636 G(4) = 1.067 G(5) = .800
V = 5
         G(2) = 5.833 G(3) = 2.242 G(4) = 1.399 G(5) = 1.042 G(6) = .833
V = 6
                 8.000 G(3) = 2.927 G(4) = 1.761 G(5) = 1.289 G(6) = 1.029
         G(2)=
V = 7
         G(7) =
                   .857
                                       G(4) = 2.162 G(5) = 1.549 G(6) = 1.227
         G(2) = 10.500 G(3) = 3.696
V = 8
         G(7) = 1.021 G(8) = .875
         G(\ 2)=\ 13.333 G(\ 3)=\ 4.549 G(\ 4)=\ 2.594 G(\ 5)=\ 1.827 G(\ 6)=\ 1.431 G(\ 7)=\ 1.186 G(\ 8)=\ 1.016 G(\ 9)=\ .889
V=9
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```
V = 10
         G(2) = 16.500 G(3) = 5.485 G(4) = 3.059 G(5) = 2.123 G(6) = 1.643
         G(7) = 1.354 G(8) = 1.158 G(9) = 1.013 G(10) = .900
         G(2) = 20.000 G(3) = 6.504 G(4) = 3.558
V = 11
                                                    G(5) = 2.434 G(6) = 1.866
         G(7) = 1.527
                        G(8) = 1.301 G(9) = 1.137
                                                    G(10) = 1.010
V = 12
         G(2) = 23.833 G(3) = 7.607 G(4) = 4.090 G(5) = 2.763 G(6) = 2.099
         G(7) = 1.706 G(8) = 1.447 G(9) = 1.262
                                                    G(10) = 1.121 G(12) = .917
V = 13
         G(2) = 28.000
                        G(3) = 8.793
                                      G(4) = 4.656
                                                    G(5)=3.108 G(6)=2.342
         G(7) = 1.892
                        G(8) = 1.597 G(9) = 1.389
                                                    G(10) = 1.232 G(12) = 1.007
V = 14
                        G(3)=10.062 G(4)=5.255 G(5)=3.470 G(6)=2.593
         G(2) = 32.500
         G(7) = 2.084
                        G(8) = 1.751 G(9) = 1.518 G(10) = 1.344 G(12) = 1.098
         G(14) =
                  .929
V = 15
         G(2) = 37.333 G(3) = 11.415 G(4) = 5.887 G(5) = 3.848 G(6) = 2.855
         G(7) = 2.281
                        G(8) = 1.910 G(9) = 1.650 G(10) = 1.458 G(12) = 1.188
         G(14) = 1.005
V = 16
         G(2) = 42.500
                        G(3)=12.851 G(4)=6.553 G(5)=4.243 G(6)=3.126
         G(7) = 2.485

G(14) = 1.082
                        G(8) = 2.072
                                      G(9) = 1.785 G(10) = 1.573 G(12) = 1.280
                        G(16) = .938
V = 17
         G(2) = 48.000
                        G(3)=14.370
                                     G(4) = 7.252 G(5) = 4.655 G(6) = 3.406
         G(7) = 2.694
                        G(8) = 2.239
                                      G(9) = 1.923 G(10) = 1.691 G(12) = 1.372
         G(14) = 1.159 \quad G(16) = 1.004
V = 18
         G(2) = 53.833
                        G(3)=15.973
                                     G(4) = 7.984 G(5) = 5.083 G(6) = 3.696
                        G(8) = 2.409
         G(7) = 2.909
                                      G(9) = 2.064 G(10) = 1.811 G(12) = 1.465
         G(14) = 1.236
                        G(16) = 1.070
                                      G(18) = .944
V = 21
         G(2) = 73.333
                       G(3)=21.281
                                      G(4)=10.381 G(5)=6.468 G(6)=4.623
         G(7) = 3.591 G(8) = 2.944
                                      G(9) = 2.503 G(10) = 2.183
                                                                  G(12) = 1.750
         G(14) = 1.470
                       G(16) = 1.271
                                      G(18) = 1.121 G(20) = 1.003
V = 24
         G(2) = 95.833
                        G(3)=27.339
                                      G(4)=13.078 G(5)=8.004 G(6)=5.636
         G(7) = 4.327

G(14) = 1.710
                       G(8) = 3.514
                                      G(9) = 2.966 G(10) = 2.573 G(12) = 2.047
                       G(16) = 1.473
                                     G(18) = 1.298 G(20) = 1.160 G(22) = 1.050
         G(24) =
                  .958
V = 27
         G(2)=121.333
                       G(3)=34.147
                                     G(4)=16.074 G(5)=9.689 G(6)=6.734
         G(7) = 5.116
                        G(8) = 4.120
                                      G(9) = 3.455 G(10) = 2.982
                                                                  G(12) = 2.355
         G(14) = 1.956
                        G(16) = 1.680
                                      G(18) = 1.476 G(20) = 1.319
                                                                  G(22) = 1.192
         G(24) = 1.089
                        G(26) = 1.001
V = 30
         G(2)=149.833
                       G(3)=41.705
                                     G(4)=19.371
                                                    G(5)=11.524
                                                                  G(6) = 7.918
         G(7) = 5.958
                                     G(9) = 3.969
                       G(8) = 4.762
                                                   G(10) = 3.409
                                                                  G(12) = 2.672
         G(14) = 2.210
                       G(16) = 1.892
                                      G(18) = 1.658
                                                   G(20) = 1.479
                                                                  G(22) = 1.336
         G(24) = 1.219
                       G(26) = 1.121
                                      G(28) = 1.038
                                                   G(30) = .967
V = 33
         G(2)=181.333
                       G(3)=50.013
                                      G(4)=22.968
                                                    G(5)=13.510
                                                                  G(6) = 9.188
         G(7) = 6.854
                       G(8) = 5.440
                                      G(9) = 4.508
                                                   G(10) = 3.853
                                                                  G(12) = 3.000
         G(14) = 2.470
                       G(16) = 2.108
                                      G(18) = 1.843
                                                   G(20) = 1.641
                                                                  G(22) = 1.481
         G(24) = 1.350
                       G(26) = 1.242
                                      G(28) = 1.149
                                                   G(30) = 1.070
                                                                  G(32) = 1.001
V = 36
         G(2)=215.833 G(3)=59.071
                                      G(4)=26.865
                                                   G(5)=15.645
                                                                  G(6)=10.543
         G(7) = 7.804 G(8) = 6.153
                                     G(9) = 5.072 G(10) = 4.316
                                                                 G(12) = 3.339
         G(14) = 2.737
                       G(16) = 2.328
                                     G(18) = 2.031 G(20) = 1.805
                                                                  G(22) = 1.627
         G(24) = 1.482 G(26) = 1.362
                                                                  G(32) = 1.098
                                     G(28) = 1.261 G(30) = 1.174
         G(34) = 1.031 G(36) = .972
V = 39
        G(2)=253.333 G(3)=68.879
                                     G(4)=31.062 G(5)=17.930 G(6)=11.985
        G(7) = 8.807
                       G(8) = 6.902
                                     G(9) = 5.661
                                                   G(10) = 4.798
                                                                  G(12) = 3.688
                3.010
                       G(16) = 2.553
                                     G(18) = 2.222 G(20) = 1.972 G(22) = 1.775
        G(14) =
        G(24) = 1.615 G(26) = 1.484 G(28) = 1.372 G(34) = 1.122 G(36) = 1.058 G(38) = 1.001
                                     G(28) = 1.372 G(30) = 1.277 G(32) = 1.195
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G(3)=79.437
                                       G(4)=35.558
                                                      G(5)=20.365
                                                                     G(6)=13.512
V = 42
         G(2)=293.833
                                                                     G(12) = 4.048
                                                      G(10) = 5.297
         G(7)=
                 9.864
                         G(8) = 7.687
                                       G(9) = 6.274
                                                                     G(22) = 1.925
                         G(16) = 2.782
                                       G(18) = 2.417
                                                      G(20) = 2.141
         G(14) =
                  3.290
                                       G(28) = 1.485
                                                      G(30) = 1.381
                                                                     G(32) = 1.292
         G(24) = 1.750
                         G(26) = 1.606
                                                                     G(42) = .976
                                       G(38) = 1.082
                                                      G(40) = 1.026
         G(34) = 1.213
                         G(36) = 1.144
                                       G(4)=40.355
                                                      G(5)=22.951
                                                                     G(6)=15.124
                         G(3)=90.745
V = 45
         G(2)=337.333
                                                      G(10) = 5.815
                         G(8) = 8.508
                                       G(9) = 6.913
                                                                     G(12) = 4.418
         G(7) = 10.974
                         G(16) = 3.015
                                       G(18) = 2.614
                                                      G(20) = 2.312
                                                                     G(22) = 2.076
                 3.577
         G(14) =
                  1.886
                         G(26) = 1.729
                                       G(28) = 1.598
                                                      G(30) = 1.486
                                                                     G(32) = 1.389
         G(24) =
                                                      G(40) = 1.103
                                                                     G(42) = 1.049
                         G(36) = 1.229
                                       G(38) = 1.163
         G(34) = 1.304
         G(44) = 1.001
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